

System and Process Assessment Research Laboratory

# SPAR Lab

Civil, Architectural and Environmental Engineering • 103/104-E Butler-Carlton Hall

# SMART ROCK TECHNOLOGY FOR REAL-TIME MONITORING OF BRIDGE SCOUR AND RIPRAP EFFECTIVENESS - GUIDELINES AND VISUALIZATION

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**Technical Advisory Council Meeting No.2** 



### **OUTLINE OF THIS PRESENTATION**

- Localization of Smart Rock
  - Localization Algorithm
  - Experimental Validation at Bridge Site
- Smart Rock Design and Prototyping
  - Motion under Various Flow Conditions
  - Design Guidelines
  - Final Design
  - Prototyping with Concrete Encasement
- Future Tasks
  - Deployment Plan
  - Field Measurement Plan





# Localization Algorithm

- The total magnetic field (intensity) of a smart rock with embedded magnet and its surrounding ferromagnetic substances is measured with a magnetometer at various points around the smart rock.
- The ambient magnetic field of the ferromagnetic substances is measured with the magnetometer and an orientation device at the same points.
- The coordinates of the measurement points are surveyed using a survey equipment (Total Station).
- The intensity and coordinate measurements at six or more points enable the localization of the smart rock.





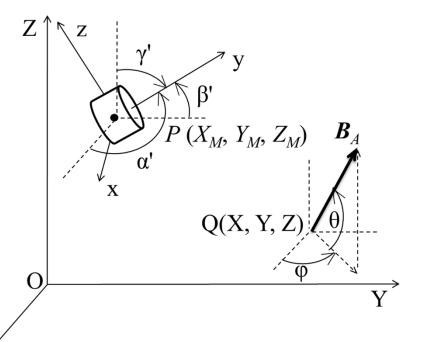
- Localization Algorithm (Cont.)
  - Ambient Field in Global XYZ Coordinate System
    - ✓ Surrounding ferromagnetic substances
    - ✓  $B_A$ = ambient magnetic field vector at a measurement point Q (X,Y,Z)
    - ✓ Three components of  $B_A$ :

$$B_{XA} = B_A \cos \theta \cos \varphi$$

$$B_{YA} = B_A \cos \theta \sin \varphi$$

$$B_{ZA} = B_A \sin \theta$$

 $\checkmark \theta(0,\pi)$  and  $\varphi(0,2\pi)$  are measured from a custom-made orientation device



- **Localization Algorithm (Cont.)** 
  - Magnetic Field of a Permanent Magnet in XYZ System
    - ✓ Cylindrical magnet  $P(X_M, Y_M, Z_M)$
    - ✓ Orientation defined in local xyz coordinate system
    - ✓ Three components of  $B_M$  at Point Q:

$$\begin{pmatrix} B_{XM} \\ B_{YM} \\ B_{ZM} \end{pmatrix} = \mathbf{T}^{-1} \begin{pmatrix} k3xy/r^5 \\ k(2y^2 - x^2 - z^2)/r^5 \\ k3zy/r^5 \end{pmatrix}$$

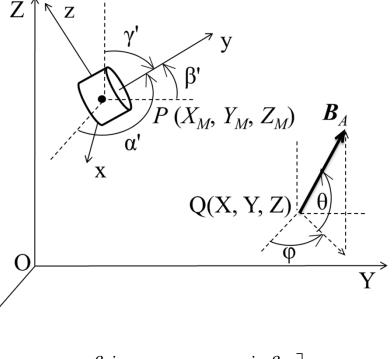
$$r = \sqrt{x^2 + y^2 + z^2}$$

$$x = a_{xX}(X - X_M) + a_{xY}(Y - Y_M) + a_{xZ}(Z - Z_M)$$

$$y = a_{vX}(X - X_M) + a_{vY}(Y - Y_M) + a_{vZ}(Z - Z_M)$$

$$z = a_{zX}(X - X_{M}) + a_{zY}(Y - Y_{M}) + a_{zZ}(Z - Z_{M})$$

$$\mathbf{T} = \begin{bmatrix} a_{xX} & a_{xY} & a_{xZ} \\ a_{yX} & a_{yY} & a_{yZ} \\ a_{zX} & a_{zY} & a_{zZ} \end{bmatrix} = \begin{bmatrix} \cos \beta \cos \gamma & \cos \beta \sin \gamma & -\sin \beta \\ \sin \alpha \sin \beta \cos \gamma - \cos \alpha \sin \gamma & \sin \alpha \sin \beta \sin \gamma + \cos \alpha \cos \gamma & \sin \alpha \cos \beta \\ \cos \alpha \sin \beta \cos \gamma + \sin \alpha \sin \gamma & \cos \alpha \sin \beta \sin \gamma - \sin \alpha \cos \gamma & \cos \alpha \cos \beta \end{bmatrix}$$



$$\cos \beta \sin \gamma \qquad -\sin \beta$$

$$\gamma \sin \alpha \sin \beta \sin \gamma + \cos \alpha \cos \gamma \qquad \sin \alpha \cos \beta$$

$$\gamma \cos \alpha \sin \beta \sin \gamma - \sin \alpha \cos \gamma \qquad \cos \alpha \cos \beta$$

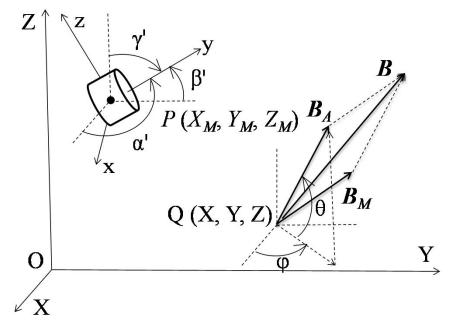




- Localization Algorithm (Cont.)
  - Total Magnetic Field at Point Q in XYZ System
    - ✓ Total magnetic field intensity:

$$B = \sqrt{(B_{XM} + B_{XA})^2 + (B_{YM} + B_{YA})^2 + (B_{ZM} + B_{ZA})^2}$$

- $\checkmark$  B = B(B<sub>A</sub>, θ, φ, k, , X, Y, Z,  $X_M$ ,  $Y_M$ ,  $Z_M$ , α, β, γ) at any measurement point Q (X,Y,Z)
- ✓ Given k,  $\theta$ ,  $\varphi$ ,  $B_A$ , X, Y, Z,  $B = B(X_M, Y_M, Z_M, \alpha, \beta, \gamma)$
- ✓ Minimum measurements at six points



- Localization Algorithm (Cont.)
  - Unknown Orientation
    - ✓ SRSS error between predicted intensity  $B_i^{(P)}$  and the measured intensity  $B_i^{(M)}$  at n measurement points

$$J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma) = \sqrt{\sum_{i=1}^{n} [B_{i}^{(P)} - B_{i}^{(M)}]^{2}}$$

$$\frac{\partial J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma)}{\partial X_{M}} = 0$$

$$\frac{\partial J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma)}{\partial Y_{M}} = 0$$

$$\frac{\partial J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma)}{\partial \alpha} = 0$$

$$\frac{\partial J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma)}{\partial \alpha} = 0$$

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$$\frac{\partial J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma)}{\partial \alpha} = 0$$

$$\frac{\partial J(X_{M}, Y_{M}, Z_{M}, \alpha, \beta, \gamma)}{\partial \gamma} = 0$$

- Known Orientation ( $\alpha$ =0,  $\beta$ =0, and  $\gamma$ =0)

$$J(X_{M}, Y_{M}, Z_{M}) = \sqrt{\sum_{i=1}^{n} [B_{i}^{(P)} - B_{i}^{(M)}]^{2}}$$

$$\frac{\partial J(X_{M}, Y_{M}, Z_{M})}{\partial Y_{M}} = 0 \qquad \frac{\partial J(X_{M}, Y_{M}, Z_{M})}{\partial Z_{M}} = 0 \qquad \frac{\partial J(X_{M}, Y_{M}, Z_{M})}{\partial X_{M}} = 0$$





- Experimental Validation at Bridge Site
  - Gasconade River Bridge Site, MO
  - Two Smart Rocks
    - ✓ Unknown orientation: Arbitrarily Oriented System (AOS)
    - ✓ Known orientation: Automatically Pointing South System (APSS)







(b) APSS

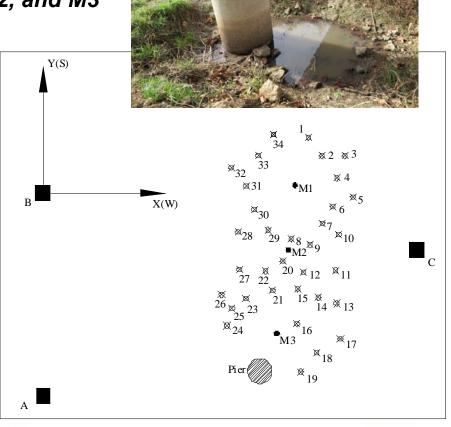




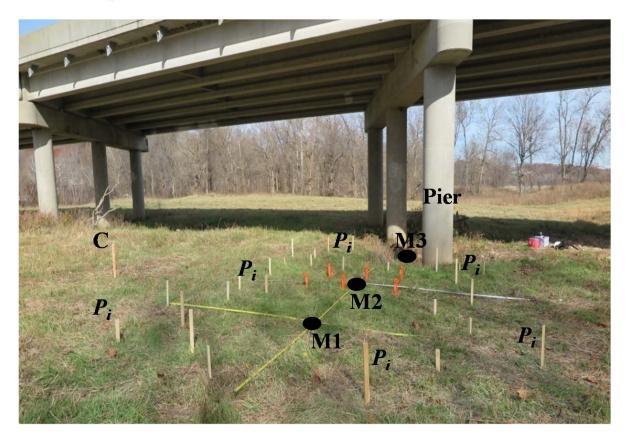
- Experimental Validation at Bridge Site (Cont.)
  - Evaluation of k,  $B_A$ ,  $\theta$  and  $\varphi$ 
    - $\checkmark$  K(AOS) = 41890.13(nT·m<sup>3</sup>), measured with high precision level
    - ✓ K(APSS) = 42542.27(nT·m³), measured with low precision level
    - ✓ Ambient magnetic field lines are no longer in parallel due to ferromagnetic substances (e.g. reinforcement in bridge pier and deck)
    - $\checkmark$  Three parameters ( $B_A$ , θ and φ) define the ambient magnetic field for each measurement point in space
      - The field intensity B<sub>A</sub> was measured with a magnetometer.
      - An Ambient Magnetic Field Orientation Device (AMFOD)
         was developed and prototyped to measure the angles θ and φ.



- Experimental Validation at Bridge Site (Cont.)
  - Test Setup around a Scour Hole
    - √ Three magnet locations M1, M2, and M3
      for AOS and APSS
    - ✓ Total 34 measurement points
    - ✓ Total Station at Point B to survey coordinates of three smart rocks and 34 sensor positions or measurement points
    - ✓ AMFOD was set at the 34 points to measure θ and φ



- Experimental Validation of at Bridge Site (Cont.)
  - Test Setup



- Experimental Validation of at Bridge Site (Cont.)
  - Test Procedure
    - ✓ Step 1: Set the Global XYZ Coordinate System
    - ✓ Step 2: Select the Locations of Smart Rocks and the Sensor Head
      - Smart rocks located far away from, near, and close to the bridge pier
      - 34 points distributed around M1, M2 and M3 bounded by circles with diameter of 1.5 m and 5 m around the pier
    - ✓ Step 3: Select a Calibration Point C for AMFOD
      - Together with a fixed object as a reference to assist in determination of angle φ
      - Set away from the 34 measurement points to ensure the line of sight from laser light to Point C

- Experimental Validation of at Bridge Site (Cont.)
  - Test Procedure (Cont.)
    - ✓ Step 4: Determine the Coordinates of Smart Rocks, Sensor Head and Calibration Point

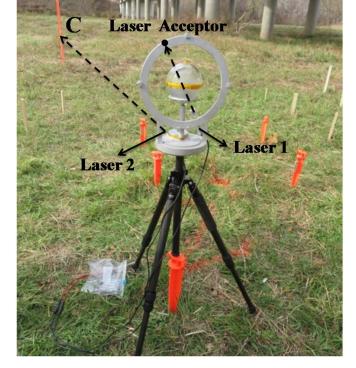




**Total Station and Prism for Positioning** 



- Experimental Validation of at Bridge Site (Cont.)
  - Test Procedure (Cont.)
    - ✓ Step 5: Measure θ and φ
      - AMFOD placed at measurement point
      - The center of high precision APSS kept along extension line of the orange plastic pole.
      - Shooting light of Horizontal Laser 2 hits on the wooden pole at Point C
      - Inside magnet automatically aligned to the ambient magnetic field
      - Shooting light of Laser 1 goes through the hole at the center line of APSS and hits on the center of laser acceptor
      - Read θ and φ





- Experimental Validation of at Bridge Site (Cont.)
  - Test Procedure (Cont.)
    - ✓ Step 6: Measure the Ambient Magnetic Field Intensity
      - Level bubble attached on the sensor head ensures the sensor perpendicular to the ground
      - Keep the center of the sensor head consistent with that of the high precision APSS by a 57.7 cm wooden pole
      - Conduct measurement without vehicles
      - At least three measurements to ensure accuracy and repeatability



Magnetometer Panel

Sensor Head





- Experimental Validation of at Bridge Site (Cont.)
  - Test Procedure (Cont.)
    - ✓ Step7 & 8: Measure the Total Magnetic Field Intensity of AOS and APSS at M1, M2 and M3





- Experimental Validation at Bridge Site (Cont.)
  - Test Results

**Table 1 Sensor Coordinates and Ambient Magnetic Field Intensities** 

	Sensor Coordinates			Ambient Magnetic Field					
Measurement Point	Schsof Coordinates			Direction			Intensity		
	<i>X</i> /m	<i>Y</i> /m	<i>Z</i> /m	$\theta$ / rad	φ / rad	$B_A$ /nT	$B_{AX}/\mathrm{nT}$	$B_{AY}/\mathrm{nT}$	$B_{AZ}/\mathrm{nT}$
С	15.284	-2.264	N/A	N/A	N/A	N/A	N/A	N/A	N/A
P1	10.882	2.202	-0.547	1.213	1.503	50798	1213	17748	47581
P2	11.425	1.481	-0.454	1.222	1.525	51417	810	17567	48316
Р3	12.365	1.479	-0.576	1.222	1.477	51363	1637	17491	48266
P4	12.040	0.587	-0.483	1.197	1.485	51366	1603	18674	47825
P5	12.701	-0.160	-0.512	1.196	1.512	51296	1102	18768	47727
•••	•••	•••	•••	•••	•••	•••	•••	•••	•••
P33	8.813	1.487	-0.724	1.143	1.511	51330	1262	21249	46709
P34	9.455	2.322	-0.436	1.162	1.410	51417	3264	20158	47188

- Experimental Validation at Bridge Site (Cont.)
  - Test Results (M1<sub>APSS</sub>)

Location of Sensor Head	X(m)	Y(m)	Z(m)	$B_{i}^{(M)}(nT)$	
P1	10.882	2.202	-0.517	58120	
P2	11.425	1.481	-0.424	56946	
	•••	•••	•••	•••	
P9	10.940	-2.065	-0.687	52055	
P10	12.119	-1.657	-0.665	50942	
P20	9.822	-2.717	-0.665	53002	
P28	7.989	-1.553	-0.659	51464	
P29	9.216	-1.476	-0.661	51031	
P30	8.651	-0.664	-0.757	48911	
	•••	•••	•••	•••	
P34	9.455	2.322	-0.406	56421	
Predicted APSS Location M1 <sub>APSS</sub>	10.249	0.454	-1.352		
Measured APSS Location M1 <sub>APSS</sub>	10.326	0.305	-1.407	N/A	
<b>Location Prediction Error for M</b> <sub>APSS</sub>	-0.077	0.149	0.055		
SRSS Error in Coordinate		0.1	76 m		





- Experimental Validation at Bridge Site (Cont.)
  - Test Results (M3<sub>APSS</sub>)

Location of Sensor Head	X(m)	Y(m)	Z(m)	$B_{i}^{(M)}(nT)$
Р9	10.940	-2.065	-0.657	52766
P11	11.991	-3.082	-0.558	52422
P12	10.670	-3.162	-0.670	55203
	•••	•••	•••	•••
P20	9.822	-2.717	-0.635	55164
P21	9.413	-3.877	-0.748	63734
P23	8.313	-4.215	-0.501	59204
P25	7.750	-4.591	-0.858	58350
P26	7.315	-4.055	-0.726	56087
P27	8.043	-3.046	-0.553	55198
Predicted APSS Location M3 <sub>APSS</sub>	9.527	-5.520	-1.850	
Measured APSS Location M3 <sub>APSS</sub>	9.576	-5.584	-1.822	N/A
<b>Location Prediction Error for M3</b> <sub>APSS</sub>	-0.049	0.064	-0.028	
SRSS Error in Coordinate		0.0851	n	

- Experimental Validation at Bridge Site (Cont.)
  - Test Results (M1<sub>AOS</sub>)

Location of Sensor Head	X(m)	Y(m)	Z(m)	$B_{i}^{(M)}(nT)$
P1	10.882	2.202	-0.517	53558
P2	11.425	1.481	-0.424	52767
•••	•••	•••	•••	•••
P9	10.940	-2.065	-0.687	49665
P10	12.119	-1.657	-0.665	49567
P20	9.822	-2.717	-0.665	51538
P28	7.989	-1.553	-0.659	50607
P29	9.216	-1.476	-0.661	48149
P30	8.651	-0.664	-0.757	47696
•••	•••	•••	•••	•••
P34	9.455	2.322	-0.406	54539
Predicted AOS Location M1 <sub>AOS</sub>	10.265	0.235	-1.456	
Measured AOS Location M1 <sub>AOS</sub>	10.326	0.305	-1.422	N/A
<b>Location Prediction Error for M1</b> <sub>AOS</sub>	-0.061	-0.070	-0.034	
SRSS Error in Coordinate		0.0	99 m	



- Experimental Validation at Bridge Site (Cont.)
  - Test Results (M3<sub>AOS</sub>)

Location of Sensor Head	X(m)	Y(m)	Z(m)	$B_{i}^{(M)}(nT)$
P9	10.940	-2.065	-0.667	52651
P12	10.670	-3.162	-0.680	54660
P13	12.031	-4.399	-0.745	52095
•••	• • •	•••	•••	•••
P20	9.822	-2.717	-0.645	54929
P21	9.413	-3.877	-0.758	62508
P23	8.313	-4.215	-0.511	59364
P25	7.750	-4.591	-0.868	59523
P26	7.315	-4.055	-0.736	56642
P27	8.043	-3.046	-0.563	55399
Predicted AOS Location M3 <sub>AOS</sub>	9.514	-5.519	-1.860	
Measured AOS Location M3 <sub>AOS</sub>	9.576	-5.584	-1.837	N/A
<b>Location Prediction Error for M3</b> <sub>AOS</sub>	-0.062	0.065	-0.023	
SRSS Error in Coordinate	0.093m			

- Motion under Various Flow Conditions
  - Criteria of Incipient Motion of Rocks
    - ✓ Critical velocity (HEC 18, 3<sup>rd</sup> version)

$$V_c = \frac{K_s^{1/2} (S_s - 1)^{1/2} d^{1/2} y^{1/6}}{n}$$

✓ Critical shear stress(HEC18, 3<sup>rd</sup> version)

$$\tau_c = K_s(\rho_s - \rho_w) gd$$

$$\tau_{local} = \left(\frac{nV_{local}}{K_u}\right)^2 \frac{\gamma_w}{y^{1/3}}$$

√ Riprap size design(HEC 23)

$$D_{50} = \frac{0.692(KV)^2}{2g(S_s - 1)}$$

- Motion under Various Flow Conditions (Cont.)
  - Incipient Motion at Various Bridge Sites
    - ✓ Highway 1 over Waddell Creek (Br. No. 36-0065)



**Highway No.1 Waddell Creek Bridge** 



- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 1 over Waddell Creek (Br. No. 36-0065)(Cont.)
      - Located about 17miles north of the city of Santa Cruz
      - Build in 1947, 4-span structure with total 180.8ft long and 31.7ft wide
      - Continuous reinforced concrete (RC) T-girders supported on RC piers and seat-type abutments
      - Up stream of the bridge, small mountain dominates the terrain; down stream, the channel alignment changes with flow intensity towards the Pacific Ocean
      - In Feb,2000, high flows from a storm caused severe erosion to the upstream channel banks and extending to the embankment at Abutment 1. Some piles at Pier 2 was exposed.
      - Then, classified as scour critical

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 1 over Waddell Creek (Br. No. 36-0065)(Cont.)
      - The 100-year flood discharge (Q100) is 170 m<sup>3</sup>/s estimated from the regional flood-frequency equation based on the historical gage data from USGS.
      - High water elevation level( HWEL) is 2.865 m during 100-year flood.
      - The flow depth (y) and velocity (V) in the directly upstream of various piers is:

Bent No.	2	3	4
y (m)	3.566	2.012	0.152
V (m/s)	2.286	3.048	1.585

 Select Bent 2 for calculation because of its unstable during 100-year flood provided by Caltrans

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 1 over Waddell Creek (Br. No. 36-0065)(Cont.)
      - Based on critical velocity (Bent 2)

$$2.286 = \frac{0.052^{1/2} \left(\frac{\rho_s}{1000} - 1\right)^{1/2} 0.25^{1/2} 3.566^{1/6}}{0.0325}, \quad \rho_s = 1278 kg / m^3$$

Where,

 $K_s$  = 0.052 for fine cobbles from the USGS Scientific Investigations Report 2008-5093;

 $S_s = \rho_s/1000$  where  $\rho_s$  is the mass density of smart rocks in kg/m<sup>3</sup>;

 $g = 9.81 \text{ m/s}^2$ ;

d = 0.25 m for smart rocks based on the required space for magnet embedment;

 $V_c = V = 2.286 \text{ m/s}$  at Bent 2;

y = 3.566 m at Bent 2;

 $n = 0.041d^{1/6} = 0.0325.$ 



- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 1 over Waddell Creek (Br. No. 36-0065)(Cont.)
      - Based on riprap size (Abutment 5)

$$0.25 = \frac{0.692(1.7 \times 1.585)^2}{2 \times 9.81 \left(\frac{\rho_s}{1000} - 1\right)}, \qquad \rho_s = 2024 kg / m^3$$

Where,

 $D_{50} = 0.25 m;$ 

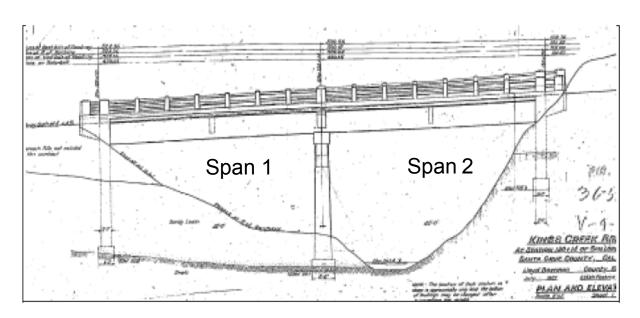
K=1.7 for a rectangle pier;

V = 1.585 m/s at Bent 4;

 $S_s = \rho_s/1000$  in kg/m<sup>3</sup>; and

 $g = 9.81 \text{ m/s}^2$ .

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 9 over Kings Creek (Bridge No.36-0054)



Schematic view of Kings Creek Bridge No.36-0054



- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 9 over Kings Creek (Bridge No.36-0054)(Cont.)
      - 2-span structures in Santa Cruz County over the Kings Creek
      - Located at the apex of a bend, main channel flow under span 2
      - Classified as scour critical in 2004 and footing pads at Bent 2 were exposed
      - A 2D hydraulic model of the flow was established by Caltrans to determine hydraulic parameter
      - The 100-year flood discharge (Q100) is 76.693 m<sup>3</sup>/s.
      - The flow depth (y) and velocity (V) was estimated as 0.3 m/s and 0.18m, respectively, at Bent 2.

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ Highway 1 over Waddell Creek (Br. No. 36-0065)(Cont.)
      - Based on critical velocity (Bent 2)

$$0.2 = \frac{0.052^{1/2} \left(\frac{\rho_s}{1000} - 1\right)^{1/2} 0.25^{1/2} 0.18^{1/6}}{0.0325}, \quad \rho_s = 1006 \, kg \, / \, m^3$$

Where,

 $K_s$  = 0.052 for fine cobbles from the USGS Scientific Investigations Report 2008-5093;

 $S_s = \rho_s/1000$  where  $\rho_s$  is the mass density of smart rocks in kg/m<sup>3</sup>;

 $g = 9.81 \text{ m/s}^2$ ;

d = 0.25 m for smart rocks based on the required space for magnet embedment;

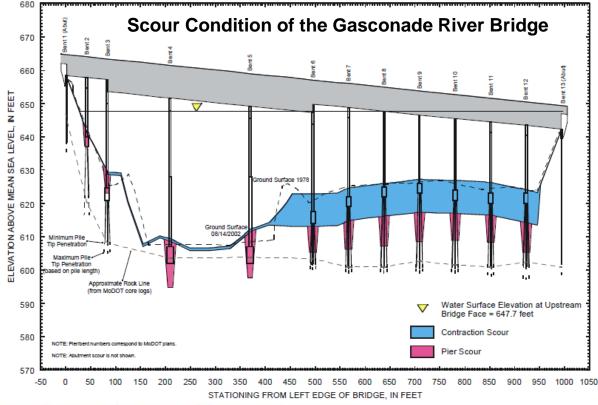
 $V_c = V = 0.2 \text{ m/s at Bent 2};$ 

y = 0.18 m at Bent 2;

 $n = 0.041d^{1/6} = 0.0325$ .



- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ US63 Gasconade River Bridge





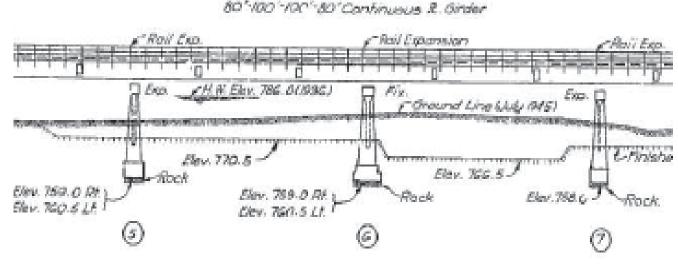


- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - √ US63 Gasconade River Bridge(Cont.)
      - Located approximately 5.5 miles southeast of Vienna in Maries County,
         MO.
      - Built in 1970's, 12-span concrete-girder Structures.
      - Bent 4 is potentially scour critical.
      - The 100-year flood discharge(Q100 = 146000 cfs = 4234 m³/s)
         estimated from historical data recorded from USGS gage station at
         Jerome, MO( gage No. 06933500).
      - The cross sectional area (A) was estimated to be 36544 ft<sup>2</sup> (3395 m<sup>2</sup>).

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ US63 Gasconade River Bridge(Cont.)
      - The average channel velocity,  $V_{average} = Q_{100} / A = 1.218 \text{ m/s}.$
      - The velocity upstream of bent 4,  $V=1.7\ V_{average}$  considering pier in the main current of flow around a bend.
      - Flow depth at Bent 4 is approximately 40ft (12.192m).
      - Therefore, with same size of 0.25m, the density is:

$$1.218 \times 1.7 = \frac{0.052^{1/2} \left(\frac{\rho_s}{1000} - 1\right)^{1/2} 0.25^{1/2} 12.192^{1/6}}{0.0325}, \quad \rho_s = 1151 kg / m^3$$

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ I-44 Roubidoux Creek Bridge (Bridge No.L0039)



GENERAL ELEVATION

Schematic view of I-44 Roubidoux Creek Bridge at Bents 5-7





- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ I-44 Roubidoux Creek Bridge (Bridge No.L0039)(Cont.)
      - Located about 12 miles south of Crocker in Pulaski County, MO.
      - 10-spans with main flow going between Bents 5 and 7
      - Bent 6 is potentially scour critical.
      - The maximum discharge and flow depth (Q<sub>max</sub> = 18200 cfs = 515.4 m³/s and y=18.70 ft= 5.70 m) recorded at the USGS gage station (USGS 0698300, Roubidoux Creek above Fort Leonard Wood, MO).
      - The cross sectional area (A) was estimated to be 11703 ft<sup>2</sup> (1087 m<sup>2</sup>).

- Motion under Various Flow Conditions(Cont.)
  - Incipient Motion at Various Bridge Sites(Cont.)
    - ✓ I-44 Roubidoux Creek Bridge (Bridge No.L0039)(Cont.)
      - The average channel velocity,  $V_{average} = Q_{max}/A = 0.474$  m/s.
      - The velocity upstream of bent 4,  $V=1.7\ V_{average}$  considering pier in the main current of flow around a bend.
      - Therefore, with same size of 0.25m, the density is:

$$0.474 \times 1.7 = \frac{0.052^{1/2} \left(\frac{\rho_s}{1000} - 1\right)^{1/2} 0.25^{1/2} 5.70^{1/6}}{0.0325}, \quad \rho_s = 1030 \, kg \, / \, m^3$$

#### Design Guidelines of Smart Rocks

- Introduction
  - ✓ Passive smart rocks embedded with permanent magnets, and remotely located with one or several magnetometers
  - ✓ Active smart rocks embedded with electronic device, and located from a remote measurement through wireless communication
  - √ Properly designed smart rocks
  - ✓ Onset movement of riprap slope protection
  - √ Maximum scour depth

#### Design Guidelines of Smart Rocks

- Design Considerations
  - ✓ Meet two requirements
    - Facilitate remote measurement for rock localization
    - Ensure automatic movement to the bottom of a scour hole to be monitored
  - √ The size of smart rock is constrained by minimum size of permanent magnet
  - ✓ Always stay at the river bed
  - ✓ Overcome water current and roll down the slope of a scour hole
  - ✓ Remain at the bottom of the hole
  - ✓ Density of smart rocks range from that of water and rocks
  - ✓ Size and density highly depend on critical velocity and depth of water flow

✓ Use 
$$d = \frac{(nV_c)^2}{K_s y^{1/3} (S_s - 1)}$$
 and  $D_{50} = \frac{0.692(KV)^2}{2g(S_s - 1)}$ 



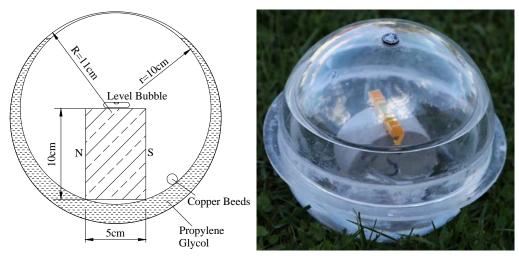
#### Design Guidelines of Smart Rocks

- Design Procedure
  - ✓ Step 1: Determine hydraulics parameters near a bridge site
    - Flow velocity and water depth directly upstream of piers for 100-year flood
    - Collected from hydraulic studies by USGS or FEMA
    - Estimated from the data recorded by USGS gage station
  - ✓ Step 2: Constrain the size and density of a smart tock
    - Inversely proportional relation between size and density
    - Given density, find out the size
    - Given size, find out density (preferred because of the embedded object)
  - ✓ Step 3:Finalize the design of smart rocks
    - Multiply by a design factor(1.2-1.3) to account for any potential errors
    - Consider the easy of deployment and fabrication

#### Final Design of Smart Rocks

- Size and Density
  - ✓ Diameter of 0.25m based on standard mold size
  - ✓ Multiply by 1.2 or 1.3 times to avoid washing away
  - ✓ Highway 1 Waddell Creek Bridge: 1.2×1278 = 1530 kg/m³
  - ✓ Highway 9 Kings Creek Bridge: 1.3×1006 = 1308 kg/m³
  - ✓ US63 Gasconade River Bridge: 1.3×1151 = 1496 kg/m³
  - ✓ *I-44 Roubidoux Creek Bridge:* 1.3×1030 = 1339 kg/m<sup>3</sup>
  - ✓ The target density of smart rocks: 1530 kg/m³

- Final Design of Smart Rocks (Cont.)
  - Internal Configuration (APSS)
    - √ Monitored along the river bank
    - ✓ Measurement station in South or North pole of the magnet
    - √ Rapid convergence and high accuracy of APSS location
    - √ However, easy affected by ferromagnetic substance



**APSS Model of Smart Rocks** 



- Final Design of Smart Rocks (Cont.)
  - Internal Configuration (APUS)
    - ✓ Automatically Pointing Upward System (APUS)
    - ✓ Magnetometer set on the bridge deck, measurement station in south pole of the magnet
    - √ Two poles of magnet aligned with vertical sensor of the magnetometer
    - ✓ Gravity-orientated direction, reduces the degree of freedom, less effect by ferromagnetic substance



(a) Schematic View (b) Prototype Smart Rock (c) Balanced Magnet APUS Model of Smart Rocks





#### Final Design of Smart Rocks (Cont.)

#### Design Details

A cylindrical magnet placed in side an organic glass ball(inside ball), an outside organic glass ball, liquid filled in between two balls, and a concrete shell encasement. Inside ball floating inside the outside ball.

#### ✓ Diameter Selection

- Magnet: 10 cm in diameter and 5cm in height
- Inside ball: 20 cm based on availability of casting molds, smart rock size and floating requirement
- Outside ball: 21 cm based on sufficient spacing for lubrication

#### √ Liquid Selection

- No friction force on the inside ball
- Nontoxicity requirement
- Density greater than 850 kg/m<sup>3</sup>
- Therefore, propylene glycol with 1040kg/m<sup>3</sup>



- Final Design of Smart Rocks (Cont.)
  - Effect of Deposit Resetting



**Overall Arrangement of Resetting Tests** 

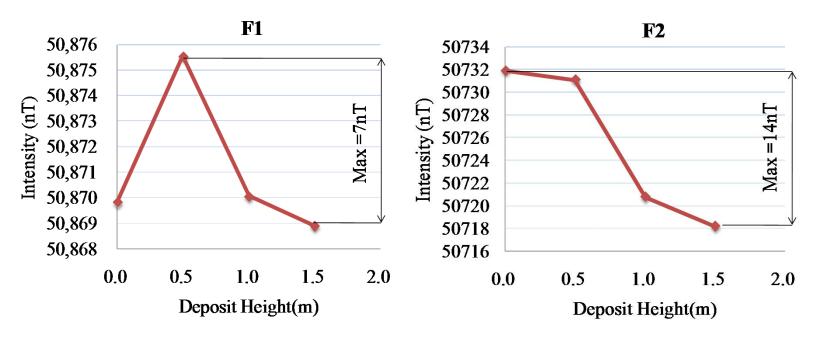


- Final Design of Smart Rocks (Cont.)
  - Effect of Deposit Resetting (Cont.)





- Final Design of Smart Rocks (Cont.)
  - Effect of Deposit Resetting (Cont.)



The intensity variations at different heights for measurement F1 and F2





- Final Design of Smart Rocks
  - Effect of Steel Reinforcement
    - ✓ Bubble in the center 10m away from the bridge pier
    - ✓ Bubble slightly deviated, indicating an inclination angle of less than 0.5 °





The Prototype APUS Placed next to a Bridge Pier



- Final Design of Smart Rocks
  - Effect of Steel Reinforcement (Cont.)
    - ✓ Little effect on the localization of the APUS





The Prototype APUS Placed on a Bridge Foundation



### Prototyping with Concrete Encasement

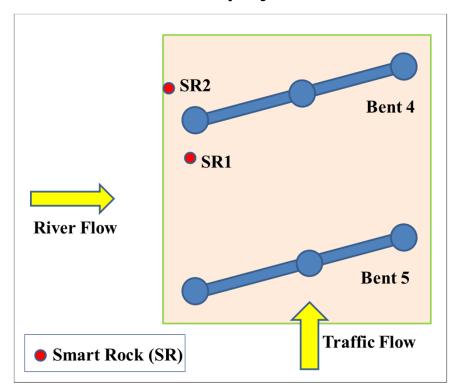
- Spherical concrete encasement
- 25-cm-diameter mold
- Close to the target value of 1530 kg/m³
- Total density is 1520 kg/m³, appropriated for Highway 1 Waddell Creek Bridge, Highway 9 Kings Creek Bridge, US-63 Gasconade River Bridge and I-44 Roubidoux Creek Bridge



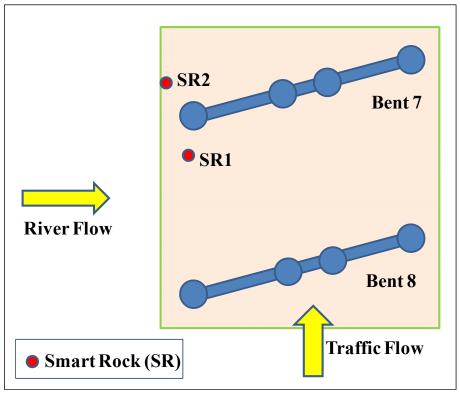
A Prototype Smart Rock



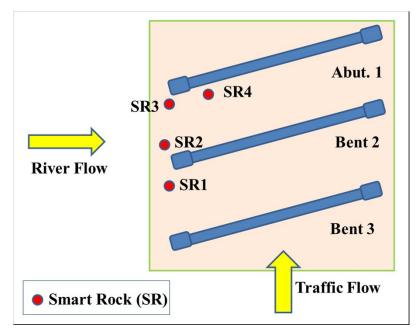
- Deployment of Smart Rocks
  - US 63 Gasconade River Bridge
    - √ The exact location of smart rocks (SR1, SR2) around Pier 4
      will be determined when deployed.



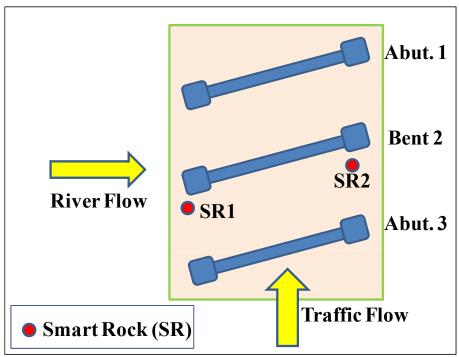
- Deployment of Smart Rocks (Cont.)
  - I-44 Roubidoux Creek Bridge
    - ✓ The exact location of smart rocks (SR1, SR2) around Pier 7 will be determined when deployed.



- Deployment of Smart Rocks (Cont.)
  - Highway 1 Waddell Creek Bridge
    - √ The exact location of smart rocks (SR1, SR2) around Pier 2
      will be determined when deployed.
    - ✓ SR3 and SR4 around abutment 1 are deployed to monitor the effectiveness of the riprap measure.



- Deployment of Smart Rocks (Cont.)
  - Highway 9 Kings Creek Bridge
    - ✓ Main flow goes through between Bent 2 and Abut.3.
    - ✓ SR1 and SR2 are in the upstream and downstream sides of the pier at Bent 2.

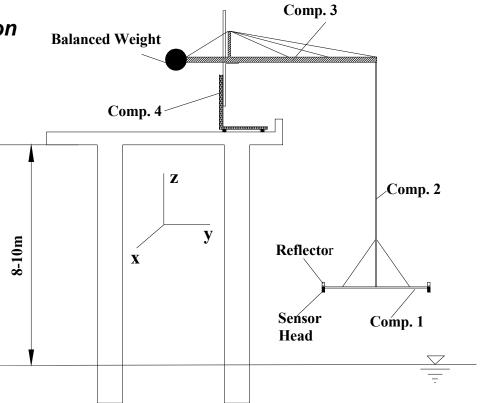


#### Measurement Plan

- Concept and Practice on Bridge Deck
  - √ Wood Frame with sensor
  - ✓ X- Longitudinal direction of the bridge
  - √ Y- Transverse direction of the bridge
  - ✓ Z- Upward
  - ✓ Movement in X-, Y-, and Z- directions
  - ✓ Measurement points distribute above the smart rocks
  - ✓ However, wood frame swung under wind load makes the difficulty to get the correct measurements.



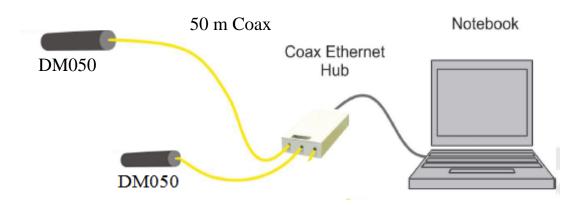
- Measurement Plan (Cont.)
  - Prototype Light Frame for Rapid Assembling on Site
    - ✓ Comp.1 Lower horizontal beam for fixing sensor (carbon fiber)
    - ✓ Comp. 2 Vertical beam (carbon fiber)
    - ✓ Comp. 3 Higher Horizontal beam (Aluminum alloy)
    - ✓ Comp. 4 Manual forklift
    - √ X-, Y-, and Z- direction
      movement by forklift





### Measurement Plan (Cont.)

- A 3 Axis Magnetometer
  - ✓ STL Digital Magnetometer (Type DM050) Measure X-, Y- and Zcomponent of any magnetic field
  - √ 50 meter Coax cable for power and data transmission
  - ✓ Interface Coax Ethernet Hub for connection of up to 3 magnetometers
  - ✓ STL GradMag software installed in a Notebook for full controlling of measurement, data acquisition and viewer



# **ANY COMMENTS?**

